

Calculation of reflected and transmitted powers of a metamaterial waveguide structure using MAPLE software

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ABSTRACT

Consider a waveguide structure consisting of a pair of metamaterial and dielectric slabs inserted in vacuum. A plane polarized wave is obliquely incident on it. Metamaterials (sometimes termed left-handed materials (LHMs)) are materials whose real parts of permittivity ϵ and permeability μ are both negative and consequently have negative index of refraction. The transmission of the electromagnetic waves through the structure is analyzed theoretically and numerically with the emphasis on the dissipation factor. Maxwell's equations are used to determine the electric and magnetic fields of the incident waves in each region. Then, Snell's law is applied and the boundary conditions of the fields are imposed at each layer interface to obtain a number of equations with unknown parameters. The MAPLE is used to solve these equations for the unknown parameters to calculate the reflection and transmission coefficients. These coefficients are used to determine the reflected, transmitted and loss powers of the structure. In the numerical results the mentioned powers are computed and illustrated as a function of frequency, angle of incidence and slab thickness when the dissipation factor changes.

Key words: Electromagnetic waves, frequency, left-handed material, dissipation factor, refractive index, transmitted power.

1. INTRODUCTION

Metamaterials (sometimes termed left-handed materials (LHMs)) are materials whose permittivity ϵ and permeability μ are both negative and consequently have negative index of refraction. These materials are artificial and theoretically discussed first by Veselago [1] over 40 years ago. The first realization of such materials, consisting of split-ring resonators (SRRs) and continuous wires, was first introduced by Pendry [2, 3]. Regular materials are materials whose ϵ and μ are both positive and termed right handed materials (RHMs). R. A. Shelby et al [4] have studied negative refraction in LHMs. I. V. Shadrivov [5] has investigated nonlinear guided waves in LHMs. N. Garcia et al [6] have shown that LHMs don't make a perfect lens. Kong [7] has provided a general formulation for the electromagnetic wave interaction with stratified metamaterial structures. M. M. Shabat et al [8] have discussed Nonlinear TE surface waves in a left-handed material and magnetic super lattice waveguide structure. I. Kourakis et al [9] have investigated a nonlinear propagation of electromagnetic waves in negative-refraction index LHM. M. F. Ubeid et al [10] have demonstrated the effect of negative permittivity and permeability on the transmission of electromagnetic waves through a structure containing left-handed material. H. Cory et al [11] and C. Sabah et al [12] have estimated high reflection coatings of multilayered structure. Oraizi et al [13] have obtained a zero reflection from multilayered metamaterial structures.

In this paper we consider a structure consisting of LHM and dielectric slabs inserted in vacuum. A plane polarized wave is obliquely incident on it. Two cases of the LHM are considered, loss-less case and loss case. Maxwell's equations are used to determine the electric and magnetic fields in each region. Then, Snell's law is applied and boundary conditions are imposed at each interface to obtain a number of equations with unknown parameters. The equations are solved for the unknown parameters by a MAPLE software to calculate the reflection and transmission coefficients. These coefficients are used to determine the reflected, transmitted and loss powers of the structure. The effect of many

parameters like frequency, angle of incidence etc. on the mentioned powers are studied in details by changing the dissipation factor of the LHM. Throughout the computations, the frequency dependence of permittivity and permeability of the LHM are taken into account. The numerical results are in agreement with the law of conservation of energy given by [11, 14, 15]. It is also noticed that the numerical results of Figure 4 is similar to Figure 8.6 obtained by [14], this is another evidence for validity of the performed computations. The propagation of electromagnetic waves through a structure containing LHM and dielectric is considered by many previous studies. Our work is concentrated on the powers of the structure and the role of properties of the dissipation factor of LHM layer. Thus, the behavior of the powers for the incident waves against the incident angle, the frequency and LHM thickness is computed and presented in numerical results with the emphasis on the dissipation factor of the LHM.

2. THEORY

We consider four regions each with permittivity ϵ_ℓ and permeability μ_ℓ , where ℓ represents the region order. Region 1 and 4 are vacuums (ϵ_0, μ_0), Region 2 is a regular dielectric (ϵ_2, μ_2), Region 3 is a metamaterial ($\epsilon_3(\omega), \mu_3(\omega)$). A polarized plane wave in Region 1 incident on the plane $z = 0$ at some angle θ relative to the normal to the boundary (see Figure 1).

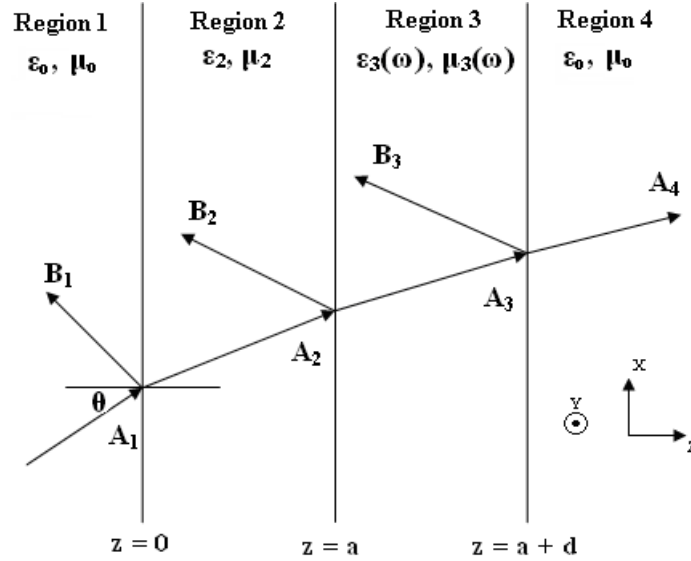


Figure 1. Wave propagation through a structure consisting of a pair of dielectric and metamaterial embedded in vacuum.

The electric field in each region is [7, 11]:

$$\vec{E}_\ell = (A_\ell e^{ik_{\ell z}z} + B_\ell e^{-ik_{\ell z}z}) e^{i(k_{\ell x}x - \omega t)} \hat{y} \quad (1)$$

We use Maxwell's equation as done by [16] to find corresponding magnetic field \vec{H}_ℓ :

$$\vec{H}_\ell = \frac{1}{\mu_\ell \omega} [(A_\ell k_{\ell x} e^{ik_{\ell z}z} + B_\ell k_{\ell x} e^{-ik_{\ell z}z}) \hat{z} + (-A_\ell k_{\ell z} e^{ik_{\ell z}z} + B_\ell k_{\ell z} e^{-ik_{\ell z}z}) \hat{x}] e^{i(k_{\ell x}x - \omega t)} \quad (2)$$

Where A_ℓ and B_ℓ are the amplitudes of forward and backward traveling waves. $k_\ell = n_\ell \omega / c$ is the wave vector inside the material and n_ℓ is the refractive index of it. Matching the boundary conditions for \vec{E} and \vec{H} fields at each layer interface, that is at $z = 0$, $E_1 = E_2$ and $H_1 = H_2$ and so on. This yields six equations with six unknown parameters [11, 13, 16]:

$$A_1 + B_1 = A_2 + B_2 \quad (3)$$

$$\frac{k_{1z}}{\mu_1}(A_1 - B_1) = \frac{k_{2z}}{\mu_2}(A_2 - B_2) \quad (4)$$

$$A_2 e^{ik_{2z}d_2} + B_2 e^{-ik_{2z}d_2} = A_3 e^{ik_{3z}d_2} + B_3 e^{-ik_{3z}d_2} \quad (5)$$

$$\frac{k_{2z}}{\mu_2}(A_2 e^{ik_{2z}d_2} - B_2 e^{-ik_{2z}d_2}) = \frac{k_{3z}}{\mu_3}(A_3 e^{ik_{3z}d_2} - B_3 e^{-ik_{3z}d_2}) \quad (6)$$

$$A_3 e^{ik_{3z}(d_2+d_3)} + B_3 e^{-ik_{3z}(d_2+d_3)} = A_4 e^{ik_{4z}(d_2+d_3)} \quad (7)$$

$$\frac{k_{3z}}{\mu_3}(A_3 e^{ik_{3z}(d_2+d_3)} - B_3 e^{-ik_{3z}(d_2+d_3)}) = \frac{k_{4z}}{\mu_4} A_4 e^{ik_{4z}(d_2+d_3)} \quad (8)$$

Where $k_{1x} = k_{2x} = k_{3x} = k_{4x} \equiv$ Snell's law and $k_{\ell z}$ is given by:

$$k_{\ell z} = \frac{\omega}{c} \sqrt{n_{\ell}^2 - n_1^2 \sin^2 \theta_1} \quad (9)$$

Letting $A_1=1$ and solving the obtained equations for the unknown parameters enables us to calculate the reflection and transmission coefficients B_1 and A_4 [11, 16]. The reflected power R and the transmitted power T are given by [11,16]:

$$R = B_1 B_1^* , T = \left(\frac{k_{4z}}{k_{1z}} \right) A_4 A_4^* \quad (10)$$

Where B_1^* and A_4^* are the complex conjugate of B_1 and A_4 respectively.

The law of conservation of energy is given by [11, 14, 15]:

$$R + T = 1 - P_{\text{loss}} \quad (11)$$

Where, P_{loss} is the loss power due to losses in LHM.

3. THE EFFECTIVE PARAMETERS

For the LHM in region 3 we employ a dispersive one with ε_3 and μ_3 appeared in [2, 3, 16]:

$$\varepsilon_3(\omega) = 1 - \frac{F_e \omega_{ep}^2}{\omega^2 - \omega_{eo}^2 + i\gamma_e \omega} \quad (12)$$

$$\mu_3(\omega) = 1 - \frac{F_m \omega_{mp}^2}{\omega^2 - \omega_{mo}^2 + i\gamma_m \omega} \quad (13)$$

where ω_{ep} and ω_{mp} are the electric and magnetic plasma frequencies, ω_{eo} and ω_{mo} are the electric and magnetic resonance frequencies. F_e and F_m are the scaling filling parameters. γ_e and γ_m are the electric and magnetic dissipation factors. We have used the following parameters appearing in [16]: $\omega_{mp} = 2\pi \cdot 10.95$ GHz, $\omega_{mo} = 2\pi \cdot 10.1$ GHz, $F_m = .26$, $\omega_{ep} = 2\pi \cdot 13.3$ GHz, $\omega_{eo} = 2\pi \cdot 10.3$ GHz, $F_e = .37$. The electric and dissipation factors are selected to be equal to each other ($\gamma_e = \gamma_m = \gamma$) and two cases of the LHM are considered, loss-less case ($\gamma = 0$) and loss_case ($\gamma \neq 0$). The operating frequency is assumed to be $f_o = 11$ GHz. This frequency is chosen by an arbitrary decision, but it must be in the frequency band where the permittivity and permeability of the LHM are both simultaneously negative. Region 1, 2 and 4 in Fig. 1 are assumed to be loss-less and the permeability's of them are equal to the permeability of free space. The refractive index of the dielectric in region 4 is selected to be 1.883. The thickness of each of LHM and dielectric slabs is equal to one half-wavelength long at the operating frequency.

4. CONSTRUCTION OF THE PROGRAMME

In this section the MAPLE programme is constructed as follows (note that, only the blue and red items appear in the programme):

- Input

The thickness of the slabs (a, d), the velocity of light ($c = .3$ Gm/sec) as well as the constant π :

```
> a:=.0135;d:=.0135;pi:=22./7.;c:=.3:
a := .0135
d := .0135
```

The frequency and the angle of incidence:

```
> th:=30.*(22/7)/180.;w:=2.*pi*11.;;
w := 69.14285715
```

The constants γ_m , γ_e , F_m , ω_{mp} and ω_{m0} :

```
> gamam:=.1:gamae:=.1:fm:=.26:wmp:=2.*pi*10.95:wmo:=2.*pi*10.1:
```

The permeability μ_3 :

```
> mu3:=1.-fm*wmp^2/(w^2-wmo^2+I*gamam*w);;
mu3 := -.641495669 + .01512700063 I
```

The permeabilities μ_1 , μ_2 , and μ_4 :

```
> mu1:=1.:mu4:=1.:mu2:=1.:
```

The constants F_e , ω_{ep} and ω_{e0} :

```
> fe:=.37:wep:=2.*pi*13.3:w eo:=2.*pi*10.3:
```

The permittivity ϵ_3 :

```
> eps3:=1.-fe*wep^2/(w^2-weo^2+I*gamae*w);;
eps3 := -3.389019785 + .05151431672 I
```

The refractive index n_3 :

```
> n31:=sqrt(mu3*eps3);;
n31 := 1.474476067 - .02859046592 I
> n32:=-sqrt(mu3*eps3);;
n32 := -1.474476067 + .02859046592 I
```

To choose the negative sign of n_3 if ϵ_3 and μ_3 are both negative:

```
> n3:=1*(0 + `if`(Re(mu3)<0,n32,n31));;
n3 := -1.474476067 + .02859046592 I
```

The refractive indices n_1 , n_2 and n_4 :

```
> n1:=1.:n2:=1.883:n4:=1.:
```

The wave vector components in the z direction:

```
> k1z:=(w/c)*sqrt(n1^2-n1^2*sin(th)^2);;
k1z := 199.5739453
> k2z:=(w/c)*sqrt(n2^2-n1^2*sin(th)^2);;
k2z := 418.3956406
> k3z1:=(w/c)*sqrt(n3^2-n1^2*sin(th)^2);;
k3z1 := 319.6899492 - 7.004580197 I
> k3z2:=-w/c)*sqrt(n3^2-n1^2*sin(th)^2);;
k3z2 := -319.6899492 + 7.004580197 I
> k3z:=1*(0 + `if`(Re(mu3) < 0,k3z2,k3z1));;
k3z := -319.6899492 + 7.004580197 I
> k4z:=(w/c)*sqrt(n4^2-n1^2*sin(th)^2);;
k4z := 199.5739453
```

The equations 3-8 are inserted:

```
> solve({A1+B1=A2+B2,k1z/mu1*(A1-B1)=k2z/mu2*(A2-B2),A2*exp(I*k2z*a)+B2*exp(-I*k2z*a)=A3*exp(I*k3z*a)+B3*exp(-I*k3z*a),k2z/mu2*(A2*exp(I*k2z*a)-B2*exp(-I*k2z*a))=k3z/mu3*(A3*exp(I*k3z*a)-B3*exp(-I*k3z*a)),A3*exp(I*k3z*(a+d))+B3*exp(-I*k3z*(a+d))=A4*exp(I*k4z*(a+d)),k3z/mu3*(A3*exp(I*k3z*(a+d))-B3*exp(-I*k3z*(a+d)))=k4z/mu4*A4*exp(I*k4z*(a+d)),A1=1}, {A1,B1,A2,B2,A3,B3,A4});
```

- Output

```

{A1 = 1., A3 = -.4690588276 - .3173894691 I,

B2 = -.2003993921 + .1272281172 I,

A2 = .5749411686 + .04505120142 I,

B1 = -.6254582235 + .1722793186 I,
A4 = -.4375718935 + .5066159969 I,

B3 = .09541542297 - .1359450003 I}

> b1:=-.6254582235+.1722793186*I;
> b1conj:=conjugate(b1);
      b1conj := -.6254582235 - .1722793186 I
> R:=b1*b1conj;
      R := .4208781530
> a4:=-.4375718935+.5066159969*I;
      a4 := -.4375718935 + .5066159969 I
> a4conj:=conjugate(a4);
      a4conj := -.4375718935 - .5066159969 I
> T:=(k4z/k1z)*a4*a4conj;
      T := .4481289303
> ploss:=1.0-(R+T);
      ploss := .1309929167

```

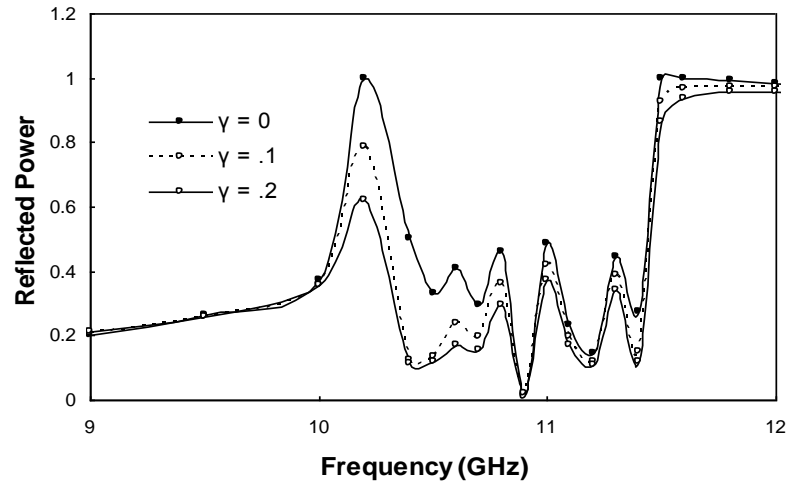
5. NUMERICAL RESULTS

In figure 2 we show a calculation of reflected, transmitted and loss powers of the considered structure as a function of frequency for three values of dissipation factor of the LHM ($\gamma = 0, .1$ and $.2$ GHz) and for 30° angle of incidence. The frequency is changed between 9 GHz and 12 GHz, because the simultaneously negative permittivity and permeability can be realized in this range in all cases, according to Eq (12) and (13). As confirmed from Fig. 2, the powers show increasing, decreasing and oscillatory behaviors in different frequency ranges. The interpretation of this is as follows: the transmission is null above 11.5 GHz frequency, where all incident radiation is being reflected. In this band $\epsilon_3(\omega)$ and

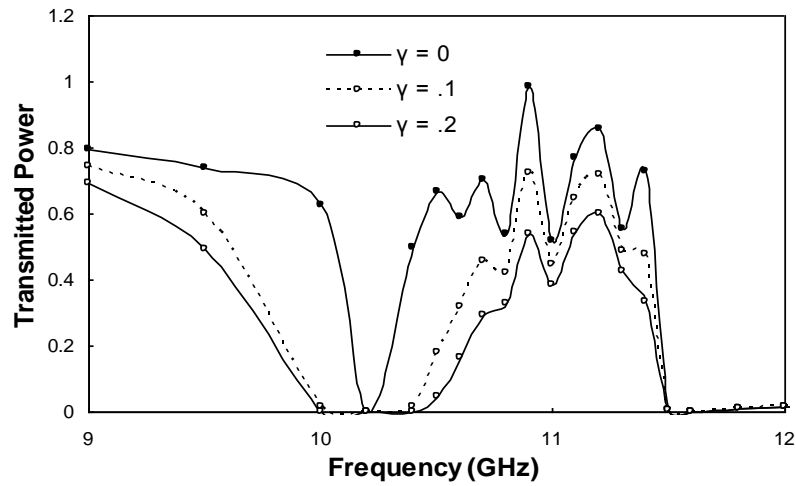
$\mu_3(\omega)$ are different in signs, and then n_3 is imaginary, this is because $n_3 = \sqrt{\epsilon_3 \mu_3 / \epsilon_0 \mu_0}$. In 10.3-11.5 GHz band the

transmission is very good. In this band $\epsilon_3(\omega)$ and $\mu_3(\omega)$ are both negative, and then n_3 is real. At 10.1 and 10.2 GHz frequencies the transmitted power is zero because $\mu_3(\omega)$ is positive and $\epsilon_3(\omega)$ is negative and then n_3 is imaginary. In 9-10 GHz band the transmitted power is not zero because both $\epsilon_3(\omega)$ and $\mu_3(\omega)$ are positive and then n_3 is real. This means that electromagnetic waves will only propagate in a medium that has a real index of refraction [16]. This interpretation is presented for loss-less case and can be applied on the loss case of LHM.

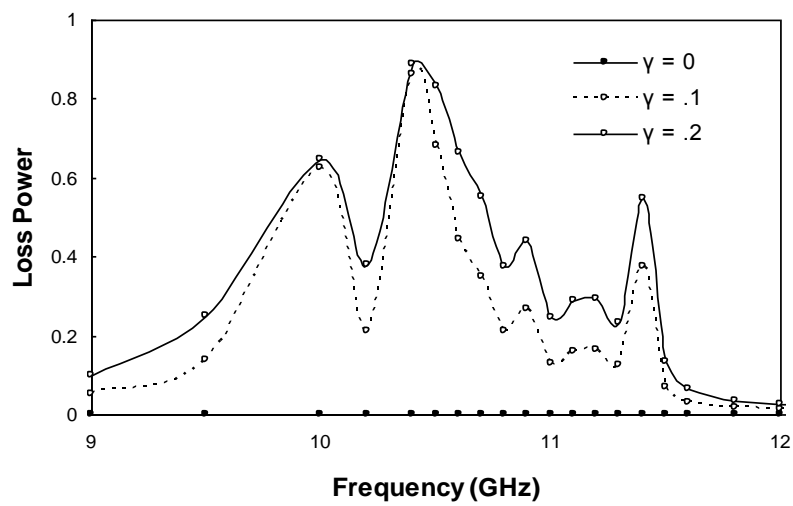
Figure 3 illustrates the variation of reflected, transmitted and loss powers with the angle of incidence. The angle of incidence is changed between 0° and 90° to realize all possible angles of incidence. Clearly the reflected power increases while the transmitted and loss powers decrease with the angle of incidence. At 90° the reflected power is maximum while the transmitted and loss powers are minimum at that angle for any value of dissipation factor. The role of the dissipation factor is clear at angles below 90° . The reflected and transmitted powers decrease while the loss power increases with the dissipation factor for any angle below 90° .



(a)

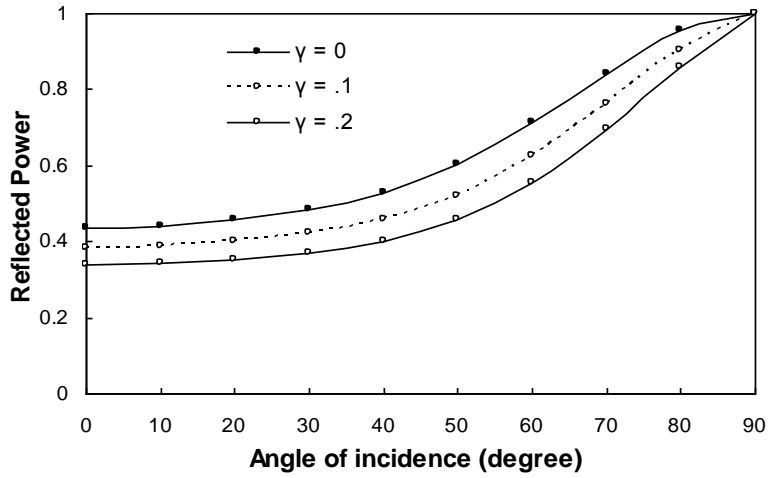


(b)

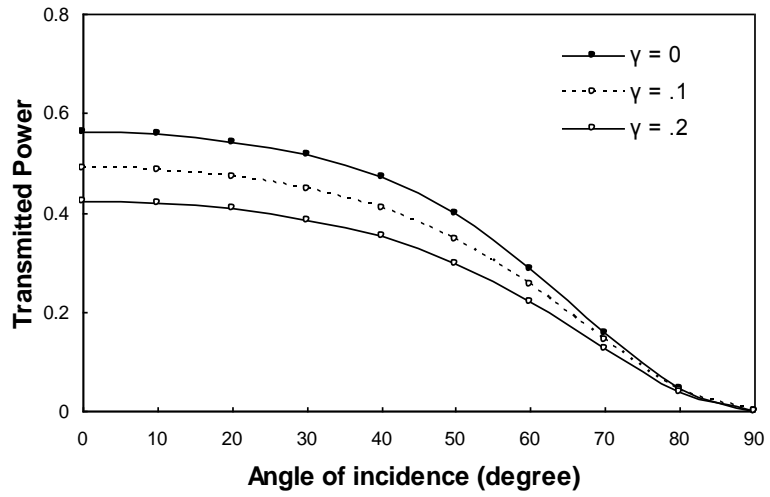


(c)

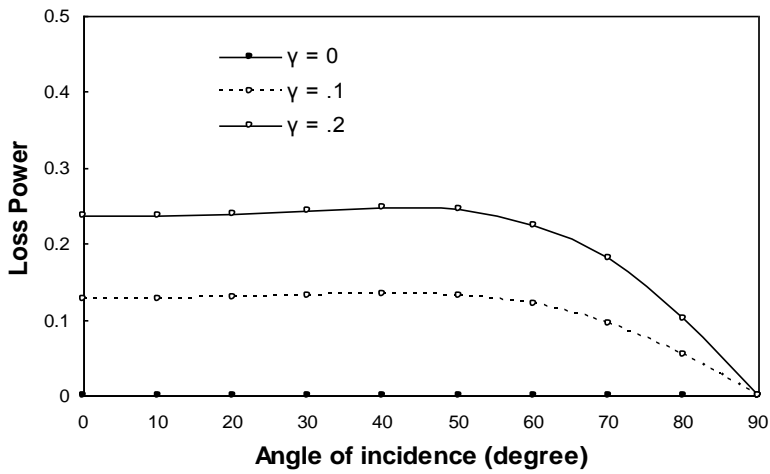
Figure 2 . Reflected, transmitted and loss powers as a function of frequency.



(a)

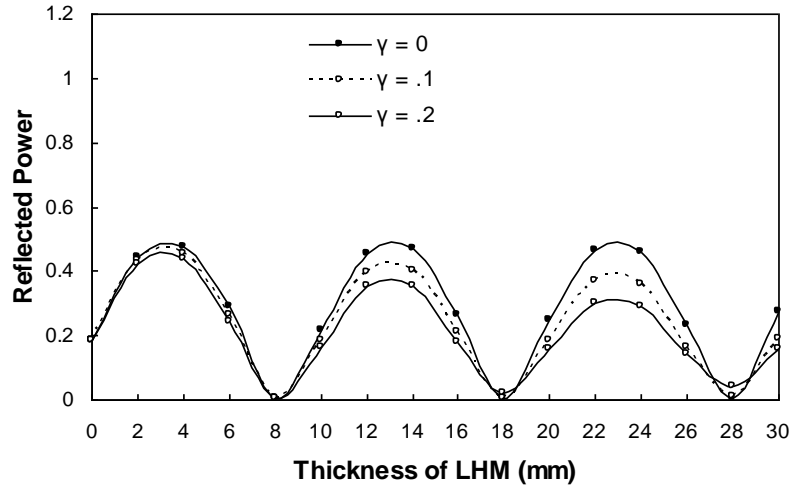


(b)

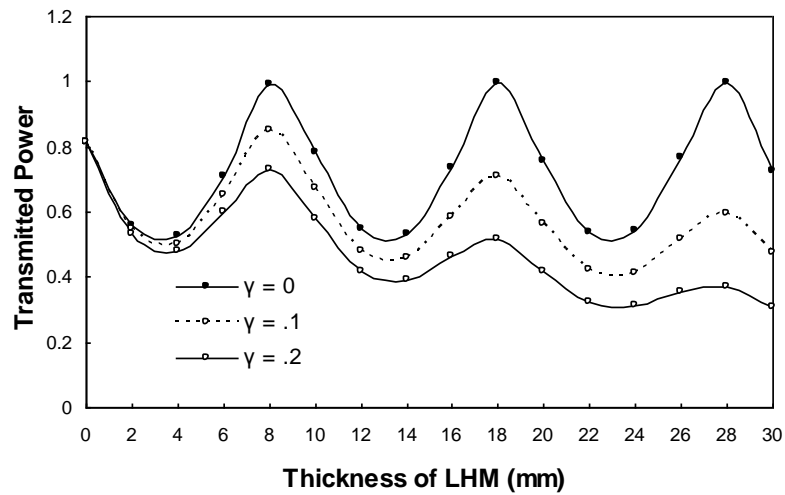


(c)

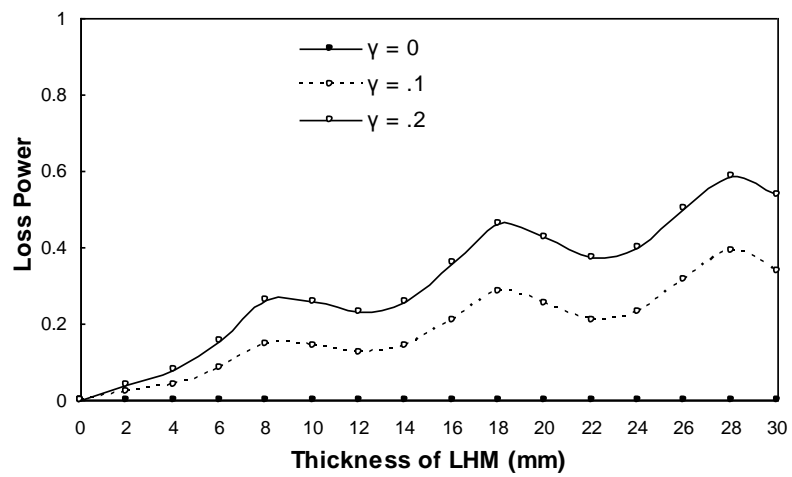
Figure 3 . Reflected, transmitted and loss powers against the angle of incidence.



(a)



(b)



(c)

Figure 4 . Reflected, transmitted and loss powers versus thickness of LHM.

Figure 4 demonstrates the effect of thickness of LHM on the reflected, transmitted and loss powers respectively at 30° angle of incidence. The slab thickness is changed from zero to 30 mm. It is noticed from the figure that the reflected power changes periodically for all dissipation factors. The transmitted power shows the same property for $\gamma = 0$ GHz, it shows oscillatory decreasing when $\gamma = .1$ and $.2$ GHz. On the other hand the loss power shows oscillatory increasing behavior with the increasing values of the dissipation factor.

6. CONCLUSIONS

A MAPLE program is designed to study the transmission and reflection of electromagnetic waves by a structure containing LHM with effect of the dissipation factor. The followed method is based on Maxwell's equations and matching the boundary conditions for the electric and magnetic fields at each layer interface. The frequency dependence of ϵ and μ of the LHM is taken into account. The dependence of the reflected, transmitted and loss powers of the considered structure on various parameters have been investigated to observe the effect of the dissipation factor. As can be seen from the numerical results, if the dissipation factor changes, the behaviors of the powers will be affected from this change. Consequently the dissipation factor has an important role in the variations of the powers. The law of conservation of energy given by [11, 14, 15] is satisfied by our results. The discussed problem is useful for applications which require controlling of reflected and transmitted powers like antenna radome, microwave, millimeter wave and optical devices

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